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# The impact of dissolved fluorine on bubble nucleation in hydrous rhyolite melts

James E. Gardner<sup>a,\*</sup>, Sahand Hajimirza<sup>b</sup>, James D. Webster<sup>c</sup>, Helge M. Gonnermann<sup>b</sup>

<sup>a</sup> Department of Geological Sciences, Jackson School of Geosciences, The University of Texas at Austin, Austin, TX 78712-0254, USA <sup>b</sup> Department of Earth Sciences, Rice University, Houston, TX 77005, USA

<sup>c</sup> Department of Earth and Planetary Sciences, American Museum of Natural History, Central Park West at 79th, New York, NY 10024-5192, USA

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### Abstract

Surface tension of hydrous rhyolitic melt is high enough that large degrees of supersaturation are needed to homogeneously nucleate H<sub>2</sub>O bubbles during eruptive magma ascent. This study examines whether dissolved fluorine lowers surface tension of hydrous rhyolite, and thus lowers the supersaturation required for bubble nucleation. Fluorine was targeted because it, like H2O, changes melt properties and is highly soluble, unlike all other common magmatic volatiles. Rhyolite melts were saturated at  $P_s = 245$  MPa with H<sub>2</sub>O fluid that contained F, generating rhyolite with 6.7  $\pm$  0.4 wt.% H<sub>2</sub>O and 1.1–1.3 wt.% F. When these melts were decompressed rapidly to  $P_f = 149-202$  MPa and quenched after 60 s, bubbles nucleated at supersaturations of  $\Delta P = P_s - P_f \ge 52$  MPa, and reached bubble number densities of  $N_B = 10^{12-13}$  m<sup>-3</sup> at  $\Delta P = 78-101$  MPa. In comparison, rhyolite saturated with  $6.34 \pm 0.09$  wt.% H<sub>2</sub>O, but only 0.25 wt.% F, did not nucleate bubbles until  $\Delta P \ge 100-116$  MPa, and even then, at significantly lower  $N_B$  ( $\le 10^{10}$  m<sup>-3</sup>). Numerical modeling of bubble nucleation and growth was used to estimate the values of surface tension required to generate the observed values of  $N_B$ . Slight differences in melt compositions (i.e., alkalinity and H<sub>2</sub>O content), H<sub>2</sub>O diffusivity, or melt viscosity cannot explain the observed differences in  $N_B$ . Instead, surface tension of F–rich rhyolite must be lower by approximately 4% than that of F–poor rhyolite. This difference in surface tension is significant and, for example, exceeds that found between hydrous basaltic andesite and hydrous rhyolite. These results suggest that is likely that surface tension for F–rich magmas, such as topaz rhyolite, is significantly lower than for F–poor magmas.

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## 1. INTRODUCTION

Gas bubbles nucleate in magma when volatiles become supersaturated in the silicate melt [\(Sparks, 1978\)](#page-7-0). In volcanic eruptions, volatile supersaturation  $(\Delta P = P_s - P)$ occurs when pressure on the magma  $(P)$  drops below the

 $*$  Corresponding author. Fax:  $+1$  512 471 9425. E-mail address: [gardner@mail.utexas.edu](mailto:gardner@mail.utexas.edu) (J.E. Gardner).

saturation pressure  $(P_s)$  of the volatile-bearing magma. The rate at which bubbles nucleate depends critically on the surface energy required to create clusters of molecules, called nuclei, of sufficient size to grow into bubbles. Surface energy, in turn, depends on the surface tension between a bubble and its surrounding medium. In the absence of solid substrates that can act as sites for nucleation, bubble nucleation will be homogeneous and nucleation rate will depend, in addition to  $\Delta P$ , on surface tension. All else being equal, a

<https://doi.org/10.1016/j.gca.2018.02.013> 0016-7037/© 2018 Elsevier Ltd. All rights reserved. small decrease in surface tension lowers the surface energy of a bubble nucleus and, consequently, produces a substantial increase in bubble nucleation rate (e.g., [Hurwitz and](#page-7-0) [Navon, 1994\)](#page-7-0).

Experimentally, it has been found that  $H_2O$  bubbles nucleate homogeneously in rhyolite melt only when  $\Delta P$ exceeds about 100–125 MPa ([Mourtada-Bonnefoi and](#page-7-0) [Laporte, 1999; Gardner and Webster, 2016](#page-7-0)). At  $\Delta P \approx 100$ –125 MPa, the induction time [\(Kashchiev, 2000;](#page-7-0) [Gonnermann and Gardner, 2013](#page-7-0)), which is the statistically averaged time required to nucleate a bubble within a given volume of melt, is longer than the typical duration of 10's to a few 100's of seconds for decompression experiments. At higher values than this critical  $\Delta P$ , the induction time becomes shorter than experimental time and thus the number of bubbles that nucleate during an experiment increases with  $\Delta P$ . Rhyolite melts that contain less than  $\sim$ 4 wt.% H2O, therefore, do not nucleate bubbles experimentally [\(Mourtada-Bonnefoi and Laporte, 1999; Gardner and](#page-7-0) [Webster, 2016\)](#page-7-0), because  $P_s \le 100-125 \text{ MPa}$  (c.f., [Liu](#page-7-0) [et al., 2005\)](#page-7-0). It has also been found that the addition of  $CO<sub>2</sub>$  to H<sub>2</sub>O-rich rhyolite does not appreciably change the induction time for bubble nucleation in rhyolite with  $\sim$ 4 wt.% H<sub>2</sub>O [\(Mourtada-Bonnefoi and Laporte, 1999;](#page-7-0) [Gardner and Webster, 2016](#page-7-0)).

The objective of this study is to examine whether the addition of fluorine (F) will significantly affect the number of bubbles nucleated in  $H_2O$ -rich rhyolite at a given value of  $\Delta P$ , all else being equal. We examine F in rhyolite because, unlike all other volatiles other than  $H_2O$ , it is highly soluble, and lowers melt viscosity and the liquidus temperature [\(Manning, 1981; Dingwell et al., 1985;](#page-7-0) [Carroll and Webster, 1994; Giordano et al., 2004; Mysen](#page-7-0) [et al., 2004; Kiprianov, 2006; Webster and Thomas, 2006;](#page-7-0) Dolejš [and Baker, 2007; Zimova and Webb, 2007;](#page-7-0) [Baasner et al., 2013](#page-7-0)). Thus, our objective is to assess whether dissolved F affects surface tension, as does  $H_2O$ [\(Gardner et al., 2013](#page-7-0)). To this end we performed a series of decompression experiments using  $H_2O$ -saturated rhyolite as a control group and compare them to a second series of decompressions that are chemically very similar, other than subtle differences in Na, Fe, and  $H_2O$  contents, except for higher concentrations of dissolved F.

#### 2. EXPERIMENTAL MATERIALS AND METHODS

All experiments used cylinders cored from a metaluminous, high-silica rhyolitic obsidian that has been used in other nucleation studies [\(Gardner, 2009; Gardner and](#page-6-0) [Ketcham, 2011; Gardner et al., 2013; Gardner and](#page-6-0) [Webster, 2016](#page-6-0)). Most cylinders were 11–13 mm long and 2.7 mm in diameter. Three cylinders and enough distilled water to ensure that the samples were fluid saturated were sealed inside Au capsules, and each capsule was placed into externally heated, cold-seal pressure vessels and run at 850 °C ( $\pm$ 5 °C) and 250 MPa ( $\pm$ 0.1 MPa) for  $\sim$ 7 days [\(Table 1\)](#page-2-0). Two other cylinders with distilled water (again, enough to ensure fluid saturation) and NaF were added to Pt capsules, and each was placed into an internally heated pressure vessel (IHPV) and run at  $\sim$ 1100 °C and

245 MPa for  $\sim$ 7 days. After each experiment, the capsule was checked that no weight was lost. When each capsule was cracked open, a separate fluid was found in each one, showing that all runs were fluid saturated. Samples were then extracted from their capsules, and sectioned into smaller samples using a slow speed saw. Each was  $\sim 0.5$  cm long and weighed  $>50$  mg. A thin wafer ( $\sim$ 1 mm thick) was also sliced from the center of each sample and used to analyze volatile contents and melt composition (see below).

Each sample used in a decompression experiment was loaded into an Au capsule, which was welded shut and placed into a cup on the end of an Inconel rod that was then inserted into a rapid-quench, cold-seal pressure vessel. The sample was held in the water-cooled region of the vessel while the pressure vessel was heated to  $850 \degree C$  [\(Table 2](#page-2-0)). The Inconel rod was then raised with an external magnet to insert the sample into the hot zone of the pressure vessel. Pressure was quickly adjusted to 251 MPa, slightly above saturation pressure to suppress any exsolution, using a hand-operated intensifier. After a sample was heated for 5 min, pressure was released quickly to a lower final pressure  $(P_f)$ , by opening the pressure vessel to a large pressure reservoir that had been set at some low pressure. This caused very rapid drops in pressure that can be timed precisely ( $\leq$ 2.5  $\pm$  0.1 s). The sample was then held at  $P_f$  before being rapidly quenched by lowering it back into the watercooled jacket. The total time that all samples spent below  $P_s$ was 60 s [\(Table 2\)](#page-2-0). When the sample was lowered, cool water replaced it in the hot zone, which heats, resulting in a near-instantaneous pressure increase. For all decompressions, pressure increased 5–6 MPa.

All samples were examined to see whether bubbles nucleated ([Fig. 1](#page-3-0)). If they had, their sizes and number density ( $N_{\rm B}$ ; in numbers m<sup>-3</sup>) were measured using a petrographic microscope.  $N_B$  was measured by selecting 4–5 areas (40  $\mu$ m  $\times$  40  $\mu$ m) in a sample and counting all bubbles that appear as the field of view is moved through it using the focusing knob of the microscope. The thickness of each volume measured, typically 800–2000 µm, was recorded by a Heidenhain focus drive linear encoder that detects the motion of the stage, and is precise to  $\pm 0.6$  µm. The typical volume analyzed was  $\sim 0.01 \text{ cm}^3$ , and so the detection limit on  $N_{\rm B}$  is  $\sim 10^8$  m<sup>-3</sup>.

Dissolved H<sub>2</sub>O contents were analyzed with a ThermoElectron Nicolet 6700 spectrometer and Continumm IR microscope. Concentrations of molecular  $(H_2O_m)$  and hydroxl  $(OH^-) H_2O$  were determined from absorbances at  $\sim$ 5250 and  $\sim$ 4500 cm<sup>-1</sup>, using white light and a  $CaF<sub>2</sub>$  beamsplitter and the model of [Zhang et al.](#page-7-0) [\(1997\)](#page-7-0). Reported  $H_2O$  contents are the averaged sums of  $H_2O_m$  and  $OH^-$  [\(Table 2\)](#page-2-0). Sample thicknesses were measured with the focus drive encoder described above.

Concentrations of major elements and F were measured in starting and run-product glasses using a JEOL JXA-8200 electron probe micro-analyzer (EPMA) and Probe For EPMA software ([Donovan, 1995\)](#page-6-0) at the University of Texas at Austin. Six analyses were measured per sample, using a  $15-kV$  and  $10-nA$  beam with a  $10-\mu m$  diameter. A mean atomic number background correction was used for all analyses. Fluorine was measured using 90 s count times,

	$G - 1590$	$G-1591$	$G - 1680$	$F=0.2$	$F=03$
SiO <sub>2</sub>	76.64	$\overline{\phantom{a}}$		75.02	75.22
TiO <sub>2</sub>	0.02			0.05	0.04
$Al_2O_3$	13.01			12.82	12.56
$FeO*$	0.80	$\overline{\phantom{a}}$		0.36	0.46
MnO	0.04			0.05	0.06
MgO	0.01			0.02	0.08
CaO	0.70			0.57	0.72
Na <sub>2</sub> O	4.02			6.31	6.06
$K_2O$	4.75	$\overline{\phantom{a}}$		4.79	4.78
H <sub>2</sub> O	$6.29 \pm 0.01$	$6.29 \pm 0.02$	$6.45 \pm 0.08$	$6.99 \pm 0.25$	$6.39 \pm 0.06$
$\mathbf{F}$	$0.25 \pm 0.02$			$1.34 \pm 0.30$	$1.10 \pm 0.18$
A/CNK	1.0			0.77	0.76
N/NK	0.56			0.67	0.66

<span id="page-2-0"></span>Table 1 Samples used in decompression experiments.<sup>a</sup>

 $^{\circ}$  G–1590, G–1591, and G–1680 are obsidian cores that were hydrated; F–02 and F–03 are obsidian cores that were hydrated and fluorinated. Major elements (normalized to 100%) and F measured by electron microprobe, with all Fe reported as FeO; oxides are in wt.%; H<sub>2</sub>O measured by FTIR. Concentrations of H<sub>2</sub>O and F are listed in wt.% with  $\pm 1$  s errors. "–" = not analyzed.

Table 2 Decompression experiments: Conditions and results.<sup>a</sup>

Run	<b>Starting</b>	$P_{\rm i}$ (MPa)	$P_{\rm f}$ (MPa)	T $(^\circ C)$	Time	F $(wt. \% )$	$log N_B$ $(m^{-3})$	d $(\mu m)$	$\sigma$ $(N m^{-1})$
	Material								
$G-1621$	$F=03$	251	222.5	850	1.0/59.0		$\theta$		
$G-1630$	$F=03$	251	202.0	850	1.9/58.1	$0.93 \pm 0.06$	$\mathbf{0}$		
$G-1618$	$F=02$	251	197.5	850	1.6/58.4	$1.21 \pm 0.16$	9.8	$11 \pm 1$	0.037
$G-1615$	$F=02$	251	172.5	850	2.0/58.0		11.8	$21 \pm 4$	0.047
$G-1629$	$F=03$	251	149.5	850	2.0/58.0	$1.27 \pm 0.18$	13.0	$8 \pm 3$	0.055
$G-1613$	$F=02$	251	149.0	850	2.0/58.0	$1.13 \pm 0.08$	11.9	$22 \pm 8$	0.056
$G-1636$	$G-1590$	251	200.0	850	1.4/58.6		$\theta$		
$G-1639$	$G-1591$	251	180.0	850	1.8/58.2	$\overline{\phantom{0}}$	$\Omega$		
$G-1611$	$G-1590$	251	173.5	850	2.0/58.0		$\theta$		
$G-1609$	$G-1590$	251	149.0	850	2.4/57.6		9.4	$54 \pm 11$	0.058
$G-1645$	$G-1591$	251	149.0	850	1.9/58.1		$\theta$		
$G-1685$	$G-1680$	251	134.0	850	1.7/58.3		9.3	$57 \pm 2$	0.065

<sup>a</sup> Compositions of starting materials are listed in Table 1.  $P_i$  and  $P_f$  = initial and final pressures of the experiment. Times are number of seconds it took to lower pressure to  $P_f(\pm 1 \text{ s})$ /number of seconds held at  $P_f$ . F (in wt.%) dissolved in glasses measured by electron microprobe ( $\pm 2$  s errors). N<sub>B</sub> is the number density of bubbles nucleated, and d is the average diameter of bubbles nucleated. "–" = not analyzed. The estimated surface tension (s) to produce the observed  $N<sub>B</sub>$  for the given decompression is given for experiments that nucleated bubbles; errors on  $\sigma$  are  $\leq 0.001$  N m<sup>-1</sup>.

with a larger (3-mm) slit size to improve counts. All other elements (Na, Mg, Al, Si, K, Ca, Mn, Fe, Ti) were measured using 20 s count times and a standard (0.3-mm) slit size. A secondary glass standard was measured periodically to ensure accuracy of the data.

### 3. EXPERIMENTAL RESULTS

Melt compositions of the starting materials differ slightly, depending on the method used (Table 1). The dissociation of NaF as the source of F enriched the melt in Na2O, which changed their alkalinity relative to those that were only hydrated, as measured by the molar ratios  $A/CNK$  [=Al<sub>2</sub>O<sub>3</sub>/(CaO + Na<sub>2</sub>O + K<sub>2</sub>O)] and N/NK  $[=Na<sub>2</sub>O/(Na<sub>2</sub>O+K<sub>2</sub>O)]$ . It also appears that some FeO was lost from the melt to the Pt tubing. Within error, most

others elements were present in all glasses at the same concentrations.

Starting materials were generated in the presence of a separate fluid of  $H_2O$  or  $H_2O+F$ , and hence all were fluid saturated. The glasses of the three samples hydrated without added NaF contain  $\sim 0.25$  wt.% F and, on average,  $6.34 \pm 0.09$  wt.% H<sub>2</sub>O (Table 1). This H<sub>2</sub>O content agrees within error of that predicted by the solubility model of [Liu et al. \(2005\).](#page-7-0) The samples hydrated and fluorinated at 1100 °C and 245 MPa contain 1.1–1.4 wt.% F. At those conditions, the model of Liu et al. predicts that  $H_2O$  solubility is  $\sim$ 0.4 wt.% lower than at 850 °C and 250 MPa. On the other hand, the data presented by [Holtz et al. \(1993\)](#page-7-0) argues that adding  $\sim 1.0$  wt.% F to the melt increases H<sub>2</sub>O solubility by  $\sim 0.4$  wt.%. Overall, therefore, samples F–02 and F–03 should have equal or slightly higher  $H_2O$ 

<span id="page-3-0"></span>

Fig. 1. Photomicrographs of representative experiments (scale bars shown in each): (a) G–1609, showing fringe bubbles that nucleated heterogeneously along the edge of the sample; (b) G–1609, showing isolated bubbles that homogeneously nucleated in F–poor rhyolite melt; (c) G–1615 and (d) G–1613, showing bubbles that nucleated in the interiors of F–rich rhyolite melts. Note the many more bubbles in (d) compared to (b), both of which decompressed to the same final pressure.

contents than those hydrated only, and indeed they contain, on average,  $6.7 \pm 0.4$  wt.% H<sub>2</sub>O [\(Table 1](#page-2-0)).

In the decompression experiments, numerous bubbles (often  $\leq 10 \mu m$ ) grew in the outer fringes of all samples (Fig. 1a). Such ''fringe" bubbles occur almost invariably in decompressions of hydrous melts, and result from heterogeneous nucleation at the contact with the metal capsule [\(Mangan and Sisson, 2000](#page-7-0)). We ignore these bubbles, and instead focus on the interiors of samples, because we are interested in the conditions needed to nucleate bubbles homogeneously in rhyolite melt (Fig. 1b). This is justified, because the characteristic diffusion length scale during the experiments is at least one order of magnitude shorter than the distance between capsule wall and sample interior.

Decompressions of hydrated rhyolites that contain  $\sim$ 0.25 wt.% F establish reference conditions ([Table 2](#page-2-0)). Bubbles nucleated in these melts only when decompressed to  $P_f = 134-149$  MPa, and thus at  $\Delta P = 101-116$  MPa (Fig. 2). Similar numbers of bubbles nucleated at these pressures, and were  $\sim$  55 µm in diameter (Fig. 1b). The absence of bubbles in sample G–1645 ( $P_f$  = 149 MPa) and low  $N_B$  values in samples G-1609 and G-1685 suggest that  $\Delta P = 101-116$  MPa was not high enough for the induction time to become significantly shorter than the experimental duration.

Hydrous rhyolites with 1.1–1.4 wt.% F were decompressed to  $P_f = 149 - 222.5 \text{ MPa}$  [\(Table 2](#page-2-0)). Four run-product glasses, three of which nucleated bubbles, were analyzed for their F contents and found to contain concentrations within error of the initial values. No bubbles nucleated at  $P_f = 202 \text{ MPa}$ , whereas bubbles nucleated in all samples decompressed to  $P_f$  <198 MPa. For these melts, therefore, the induction time becomes less than the



Fig. 2. Variations in bubble number density ( $N_B$ ; bubbles per m<sup>3</sup>) as a function of supersaturation  $(\Delta P)$ . Green diamonds are samples with  $1.1-1.3$  wt.% F; red circles are those with  $0.25$  wt.% F (F) contents are listed next to each symbol for reference). Open symbols with arrows are samples that did not nucleate bubbles ( $N<sub>B</sub>$  $= 0$ ). The approximate detection limit on bubble number density, based on the typical volume of sample measured, is  $10^8$  m<sup>-3</sup>. The dashed curves divide conditions at which bubbles nucleate versus conditions that do not generate bubbles. (For interpretation of the references to colour in this figure legend, the reader is referred to the web version of this article.)

experimental time scale when  $\Delta P$  exceeds  $\sim$  48 MPa (Fig. 2). At  $\Delta P = 77.5$ ,  $N_{\rm B} \approx 10^{12} \,\rm m^{-3}$ , and at  $\Delta P = 100$ MPa,  $N_{\rm B}$  reached  $10^{13}$  m<sup>-3</sup> (Fig. 1c and d). Importantly, at similar values of  $\Delta P$ , samples with 1.1–1.4 wt.% F

<span id="page-4-0"></span>nucleated orders of magnitude more bubbles than those with 0.25 wt.% F. The bubbles in the F–rich samples are substantially smaller than those in F–poor samples, in accord with the orders of magnitude increases in  $N<sub>B</sub>$ ([Gardner et al., 1999\)](#page-7-0).

## 4. ESTIMATION OF NUCLEATION RATE AND SURFACE TENSION

To augment the quantitative evaluation of our experimental results we modeled bubble nucleation and growth during decompression of the experimental samples. The numerical model is described in sufficient detail by [Toramaru \(1995\)](#page-7-0). We integrate the coupled ordinary differential equations for nucleation rate for bubble number density, as well as conservation of mass and momentum for bubble growth, using the MATLAB ordinary differential equation solver ode15s. In contrast to [Toramaru \(1995\),](#page-7-0) however, we used the empirical formulation for water diffusivity  $(D_{H<sub>2</sub>}$  of [Zhang and Behrens \(2000\),](#page-7-0) as well as the melt viscosity models of [Giordano et al. \(2008\)](#page-7-0). Furthermore, we used the  $H<sub>2</sub>O$  solubility model of [Liu et al.](#page-7-0) [\(2005\),](#page-7-0) adjusted for the slight increase expected as a result of added F, based on the experiments by [Holtz et al. \(1993\).](#page-7-0)

For each experiment, we estimated the value of surface tension at which the model correctly predicts the observed  $N_{\rm B}$ , assuming that surface tension is constant throughout the given experiment (Fig. 3). For those experiments where no bubbles nucleated within the sample interior we estimated the value of surface tension at which a bubble would be predicted to nucleate within the sample, which in principle corresponds to conditions where the induction time equals the time of the experiment. It should be noted that surface tension in those samples is probably higher than this minimum estimate.



Fig. 3. Estimated surface tension as a function of supersaturation pressure  $(\Delta P)$ . Symbols are the same as those in [Fig. 2](#page-3-0). Error bars (when greater than symbol size) cover the range of possible values of surface tension, assuming an order of magnitude change in  $H_2O$ diffusivity. Dashed curves connect samples that nucleated bubbles. Note that reported surface tension estimates for samples that did not nucleate bubbles are minimum values.

## 5. DISCUSSION

## 5.1. Retention or resorption of bubbles during experimental quench

After decompression and during the quench of the samples, pressure is observed to rise by 5–6 MPa as described previously. Recently, [McIntosh et al. \(2014\)](#page-7-0) found halos of glass enriched in  $H_2O$  around quenched bubbles in such experiments. They interpret such halos as recording resorption of  $H_2O$  back into the melt during cooling, and suggest that bubbles can partly resorb into the melt. Resorption occurs mainly because the solubility of  $H_2O$  increases as temperature decreases at pressures below ca. 400 MPa ([Holtz et al., 1995\)](#page-7-0) One could thus argue that the absence of bubbles in some decompressed samples is an artifact resulting from complete resorption of bubbles (with the microscope used we can identify bubbles as small as 0.5 mm in size). Two observations allow us to reject this argument. First, the same amount of resorption should occur in samples that undergo similar amounts of decompression and rate of quenching. All experiments in this study experienced similar amounts of pressure drop and the same rates of quenching ([Table 2](#page-2-0)). Bubbles exist in hydrous rhyolite melts with 1.1–1.4 wt.% F at  $P_f = 149-202$  MPa. In contrast, hydrous rhyolite melts with  $\sim 0.25$  wt.% F contain no bubbles at  $P_f > 149$  MPa. It is not tenable to suggest that bubbles had nucleated in the F–poor melts at higher pressures, only to have them all resorb completely during the quench, when the relatively F–rich melts still contain visible bubbles at pressures as high 202 MPa. Second, as previously mentioned, fringe bubbles nucleate along the melt–capsule contact during decompressions ([Fig. 1](#page-3-0)a). Those bubbles are seen in all decompressions, including those that lack bubbles in the interiors ([Fig. 1a](#page-3-0)). Again, it is not tenable to suggest that the absence of interior bubbles is an artefact of complete resorption when fringe bubbles did not resorb.

To examine this further, we modeled  $H_2O$  resorption from  $1 \mu m$  bubbles. The modeling accounted for the rate of change in temperature during sample quenching, which equals  $\sim$ 150 °C s<sup>-1</sup> ([Dobsan et al., 1990\)](#page-6-0), and the corresponding increase in solubility (following the model of [Liu et al., 2005](#page-7-0)) and decrease in diffusivity [\(Zhang and](#page-7-0) [Behrens, 2000\)](#page-7-0). We find that during quenching there could be at most a decrease on the order of 10% in mass and radius. Hence, even bubbles that were originally  $1 \mu m$  in size would still be observable in our samples. The absence of bubbles in the F–rich melts at relatively high pressures thus cannot be the result of resorption during sample quench.

## 5.2. Controls of experimental parameters on bubble nucleation

All melts were decompressed to overlapping values of  $P_f$ , the time taken to drop to  $P_f$  was the same, and all were held at  $P_f$  for the same amount of time ([Table 2\)](#page-2-0). Hence, the marked difference in  $N<sub>B</sub>$  cannot be explained by decompression conditions. There are subtle differences in melt

alkalinity, which arose from the methods used to create the starting materials [\(Table 1](#page-2-0)). It should be noted that large differences in melt composition (basaltic andesite to rhyolite) have been found to have little impact on bubble nucleation ([Gardner et al., 2013\)](#page-7-0). In this study, the  $Na<sub>2</sub>O$ contents of the melts differ by  $\sim$ 2–2.3 wt.% [\(Table 1](#page-2-0)), because F was added through dissolution of NaF. The addition of Na can affect surface tension of silicate melts, which in turn would impact the kinetics of bubble nucleation, with a decrease in surface tension promoting nucleation [\(Hurwitz and Navon, 1994; Gonnermann and](#page-7-0) [Gardner, 2013](#page-7-0)). The impact of  $Na<sub>2</sub>O$  on surface tension, however, differs for different melt compositions. In the system  $Na<sub>2</sub>O-SiO<sub>2</sub>$ , increasing the amount of Na<sub>2</sub>O increases surface tension at any given temperature ([Shartsis and](#page-7-0) [Spinner, 1951](#page-7-0)). At 1000 °C, for example, surface tension is higher by  $0.077 \text{ N m}^{-1}$  with the addition of 10 wt.% Na<sub>2</sub>O, from 20 to 30 wt.%. The impact of Na<sub>2</sub>O is similar at lower temperatures, with the addition of 2.8 wt.% Na<sub>2</sub>O (30.8–33.6) increasing surface tension by 0.003 N  $m^{-1}$  at 900 °C. In contrast, in haplogranitic melts an increase in Na<sub>2</sub>O from 4.6 to 9.0 wt.% reduces surface tension by 0.010–0.016 N m<sup>-1</sup> at temperatures above 1000 °C [\(Bagdassarov et al., 2000](#page-6-0)). Unfortunately, surface tension of relatively Na–poor haplogranitic melt was not measured at colder temperatures, but variations in surface tension with temperature for the two melts suggest that surface tension decreases more for the Na–poor melt than for the Na–enriched melt as temperature cools. In fact, the thermal variations in surface tension  $\left(\frac{d\sigma}{dT}\right)$  for the two melts predict that surface tension for the Na–enriched melt is greater by 0.002 N m<sup>-1</sup> at 850 °C, the temperature of our decompressions. [Bagdassarov et al. \(2000\)](#page-6-0) also measured surface tension for haplogranitic melt with  $20 \text{ wt.} %$  Na<sub>2</sub>O and found substantially higher surface tensions at 800–900  $\mathrm{°C}$ , supporting the conclusion that increased  $Na<sub>2</sub>O$  contents increases surface tension at temperatures equal to our decompressions. It should be noted that the predicted increase of 0.002 N m<sup>-1</sup> at 850 °C results from a difference of 5 wt.%  $Na<sub>2</sub>O$ , which is more than double the difference between our melts [\(Table 1\)](#page-2-0). We conclude that the  $\sim$ 2 wt.  $%$  difference in Na<sub>2</sub>O contents of our melts had at best no effect on surface tension, or could have even increased surface tension. Either way, the added  $Na<sub>2</sub>O$  would not promote bubble nucleation in the F-enriched melts.

Finally, there are small differences in the initial  $H_2O$ content between the starting melt compositions [\(Table 1](#page-2-0)). We included those in the modeling, but we note that they cannot account for the changes in nucleation. For example, G–1629 (F–03) contained the same amount of dissolved  $H<sub>2</sub>O$  as G-1609 and G-1645, which both lack added F, and yet G-1629 nucleated orders of magnitude more bubbles at the same value of  $\Delta P$  ([Fig. 2](#page-3-0)).

#### 5.3. Impact of fluorine on bubble nucleation

The relationships between  $\Delta P$  and  $N_B$  for both suites of experiments show that samples with greater concentrations of F produce higher values of  $N_B$  (by up to 3 orders of magnitude) at similar values of  $\Delta P$  and nucleation time ([Fig. 2](#page-3-0)).

We conclude that the increased amount of dissolved F facilitated bubble nucleation and, hence, shortened the induction time. To examine this, we calculate  $N_B$  by integrating the equation for nucleation rate, together with mass and momentum balance of the growing bubbles ([Toramaru,](#page-7-0) [1995](#page-7-0)). Nucleation rate and bubble growth are coupled through pressure and the concentration of dissolved  $H_2O$ . The nucleation rate  $(J)$  is based on classical nucleation theory and given by

$$
J = J_o \exp\left(\frac{-16\pi\sigma^3}{3kT\Delta P^2}\right) \tag{1}
$$

where k is the Boltzmann constant,  $\sigma$  is surface tension, and T is temperature. It is assumed that surface tension is constant, whereas  $\Delta P$  changes over time as a consequence of a change in pressure and in the averaged concentration of dissolved H<sub>2</sub>O. The pre-exponential term,  $J<sub>o</sub>$ , is given by

$$
J_o = \frac{n_o^2 V_m D_{\rm H_2O}}{a_o} \left(\frac{\sigma}{kT}\right)^{\frac{1}{2}}
$$
\n<sup>(2)</sup>

where  $n_0$  is the concentration of dissolved H<sub>2</sub>O molecules,  $V_{\rm m}$  is the molecular volume of H<sub>2</sub>O in the melt,  $D_{\rm H_2O}$  is diffusivity of molecular  $H_2O$  and depends on  $H_2O$  concentration, and  $a_0$  is the distance between two  $H_2O$  molecules in the melt [\(Hurwitz and Navon, 1994; Navon and](#page-7-0) [Lyakhovsky, 1998](#page-7-0)). [Navon and Lyakhovsky \(1998\)](#page-7-0) showed that  $J<sub>o</sub>$  must change many orders of magnitude in order to substantially change nucleation kinetics. Because the change in  $N_B$  between F-poor and F-rich experiments is several orders of magnitude, it is not feasible that the preexponential term  $J<sub>o</sub>$  resulted in the observed differences in nucleation rate and, hence,  $N_B$ . Furthermore, because  $[H_2O]$  is very similar in all experiments, variations in  $n_0$ or  $a_0$  are negligible. The only other non-constant parameter in  $J<sub>o</sub>$  is  $D<sub>H<sub>2</sub>O</sub>$ . Although there are no studies that have investigated the impact of [F] on  $D_{\text{H}_2\text{O}}$ , it is reasonable to assume that diffusivity may be affected by F. Changes in  $D<sub>H<sub>2</sub>O</sub>$  can also affect the rate at which supersaturation decreases as a result of H<sub>2</sub>O diffusion into nucleated bubbles. We therefore assessed the sensitivity of model predictions to the uncertainty in  $D_{\text{H}_2\text{O}}$  by systematically decreasing and increasing  $D_{\text{H}_2\text{O}}$  by one order of magnitude about the value calculated using [Zhang and Behrens \(2000\)](#page-7-0). We find that our predictions of surface tension are largely insensitive to changes in  $D_{H_2O}$  [\(Fig. 3\)](#page-4-0), supporting our hypothesis that the observed increase in nucleation rate (decrease in induction time) is a consequence of a decrease in surface tension resulting from added F.

Dissolved fluorine is known to decrease melt viscosity [\(Dingwell et al., 1985; Giordano et al., 2004\)](#page-6-0), and it has been proposed that lower viscosity leads to faster rates of bubble nucleation ([Blander and Katz, 1975](#page-6-0)). Our modeling of bubble nucleation and growth incorporates the influence of F on viscosity of the experimental melts, by using the model of [Giordano et al. \(2008\)](#page-7-0), which includes the effect of F. We find that the slight changes in viscosity that result from the differences in melt composition have minimal impact on predicted  $N_{\rm B}$ .

We thus find that the difference in  $N_B$  between F-rich and F-poor melts is consistent with a decrease in surface <span id="page-6-0"></span>tension [\(Fig. 3\)](#page-4-0). To examine this further, we focus on samples G–1609 versus G–1613, because they experienced the same decompression conditions, but yet nucleated very different numbers of bubbles [\(Table 2\)](#page-2-0). We find that the predicted value of surface tension for G–1613, with added F, is  $\approx 0.068$  N m<sup>-1</sup>, and that for G-1609, with little F, is  $\approx 0.071$  N m<sup>-1</sup>; although small, the difference is large enough to make a substantial difference in  $N_B$  [\(Fig. 3\)](#page-4-0). Overall, we conclude that the addition of F decreases surface tension between the exsolving aqueous volatile phase and the surrounding rhyolitic melt by  $\approx 4\%$  ([Fig. 3\)](#page-4-0).

#### 5.4. Implications for magmatic degassing

Magmas typically contain 100's to 1000's of ppm F (Carroll and Webster, 1994; Aiuppa et al., 2009). We found that addition of  $\leq 1$  wt.% F lowers surface tension of hydrous rhyolite melt by approximately 4% [\(Fig. 3](#page-4-0)). Even small decreases in surface tension, however, lower the surface energy of a bubble nucleus and can thus produce substantial increases in bubble nucleation rate [\(Hurwitz and](#page-7-0) [Navon, 1994](#page-7-0)). Our results thus indicate that small differences in F content may lead to substantial differences in bubble nucleation kinetics during eruptions.

Surface tension of hydrous silicate melts is also impacted by temperature and melt composition (Bagdassarov et al., 2000; Gardner and Ketcham, 2011; Gardner et al., 2013). Surface tension increases with T by  $\sim 6.9 \times 10^{-5}$  N m<sup>-1</sup>  $C^{-1}$ . Thus, to reduce surface tension as much as  $\sim$ 1 wt.% F (for rhyolite with  $\approx 6.4$  wt.% H<sub>2</sub>O), T would have to decrease by  $\sim$ 400 °C. In addition, a range of SiO<sub>2</sub> content from  $\sim$  50 to 77 wt.% resulted in surface tension for hydrous silicate melts differing by  $\leq 6\%$ , or little more than the influence of  $\sim$ 1 wt.% dissolved F. We found that the impact that dissolved F has on surface tension is in the same direction as that of added H2O (Bagdassarov et al., 2000; Gardner et al., 2013). In addition,  $H_2O$  and F have similar effects on melt properties and rheology (e.g., Dingwell et al., 1985; Baker and Vaillancourt, 1995; Giordano et al., 2004; Baasner et al., 2013). Although we do not know why dissolved F lowers surface tension, a viable hypothesis is that F dissolves into the melt by breaking bridging oxygen bonds, similar to H2O ([Mysen et al., 2004; Aiuppa](#page-7-0) [et al., 2009\)](#page-7-0). In particular, [Mysen et al. \(2004\)](#page-7-0) found that F dissolves into highly polymerized aluminosilicate melts, like that used in this study, by forming different types of Na– and Al–bearing fluoride complexes. The dissolution of F results in the depolymerization silicate melt [\(Mysen](#page-7-0) [et al., 2004; Zimova and Webb, 2007\)](#page-7-0). The effect of dissolved F on melt viscosity differs with melt composition, with the viscosity of melts that are depolymerized by other components showing little effect from added fluorine (Dingwell, 1989; Baasner et al., 2013). The solution mechanisms for fluorine in silicate melts thus depends on melt composition (Carroll and Webster, 1994). This suggests that dissolved fluorine in depolymerized melts would have less of an effect on surface tension, and thus on bubble nucleation.

Our results indicate that F–rich magmas nucleate bubbles at high rates and lower values of  $\Delta P$  compared

to F–poor magmas. Some topaz and tin rhyolites, as well as highly differentiated granitic plutons, contained >5–7 wt.% F [\(Webster and Duffield, 1994; Webster et al., 2004;](#page-7-0) [Thomas et al., 2005; Webster and Thomas, 2006\)](#page-7-0). Over a wide range of magmatic pressures, F partitioning between melt and most granitic minerals will concentrate F in the melt during magma crystallization and differentiation. Given that an increase in F of  $\sim$ 1 wt.% reduces surface tension by 4%, increasing F in the residual melt to 5–7 wt.% would probably greatly reduce surface tension. It is thus likely that highly F–enriched magmas can nucleate greater numbers of bubbles at lower degrees of supersaturation.

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